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(54) PARTIALLY RECESSED LUMINAIRE

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(51) **Int. Cl.**

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F21S 8/02	(2006.01)
F21V 21/04	(2006.01)
F21V 29/00	(2015.01)

(52) **U.S. Cl.**

CPC . ***F21S 8/02*** (2013.01); ***F21V 21/04*** (2013.01); ***F21V 29/004*** (2013.01)

(58) **Field of Classification Search**

CPC F21S 8/02; F21V 21/04; F21V 29/004
USPC 362/96, 264, 218, 294, 373, 547, 147, 362/364, 365, 366; 165/185
See application file for complete search history.

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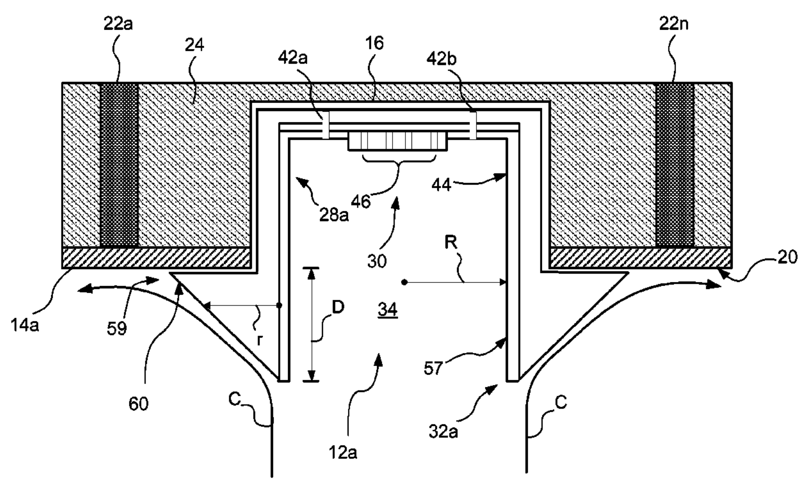
(57) **ABSTRACT**

A luminaire includes a fixture, a light engine, and a heat flange. The fixture is configured to be received in a recess of a support surface and defines a cavity having a radius R. The light engine is disposed within the cavity and includes at least one light source. The heat flange is disposed about a distal end region of the fixture and includes a hollow, generally conical frustum shape extending radially outwardly from the fixture and extending away from the distal end region of the fixture. A distal-most end of the heat flange is configured to be disposed a distance D from the support surface when the fixture is received in the recess, the distance D being greater than or equal to 0.4R. Thermal energy is conductively transferred from the light engine, through the fixture, to the heat flange where the thermal energy is convectively transferred from the heat flange to surrounding air to create air currents flowing along the support surface thereby reducing the junction temperature.

19 Claims, 16 Drawing Sheets



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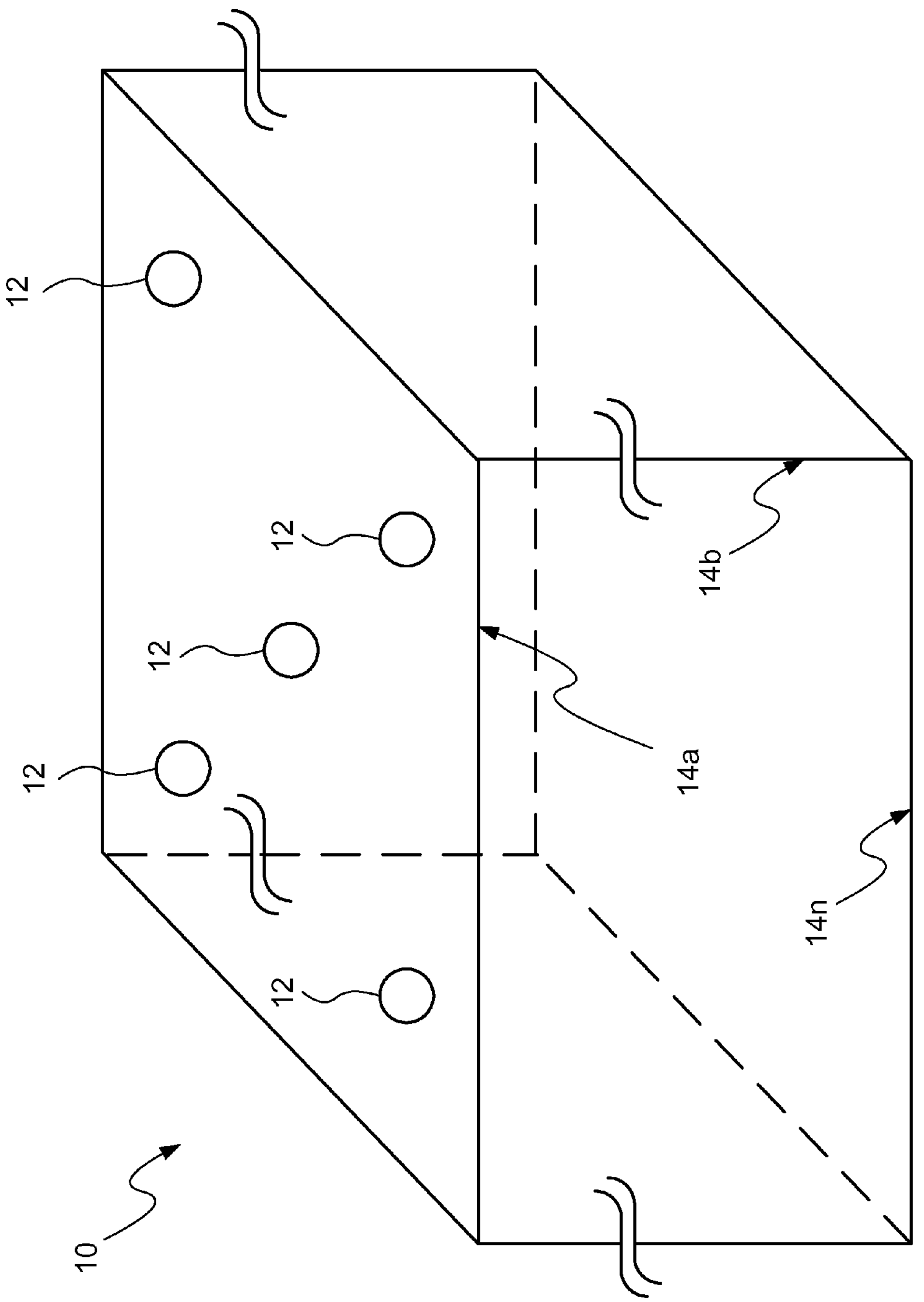
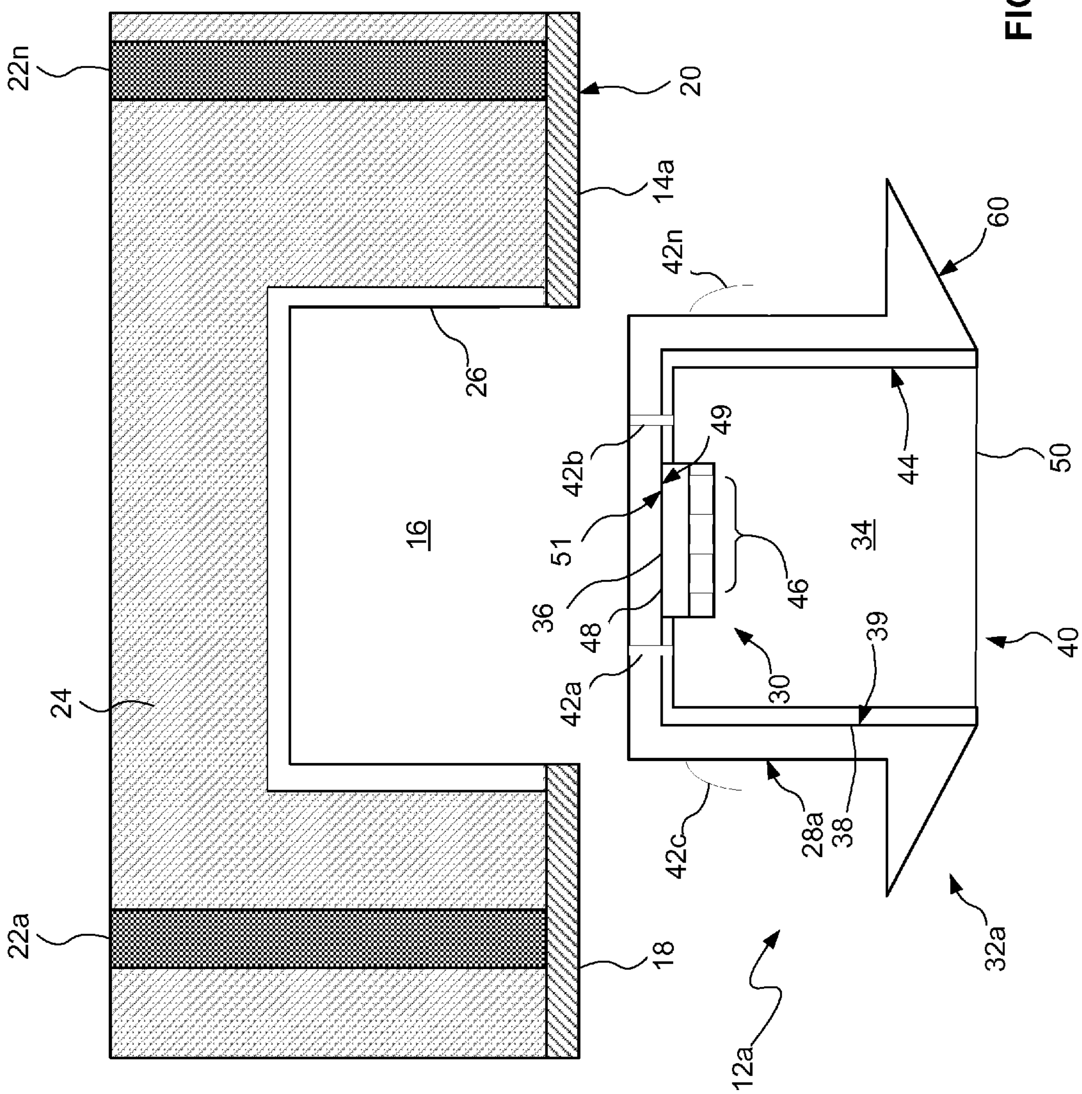


FIG. 1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20
14a
60
42n
26
49
42b
44
50
51
16
34
46
36
48
39
30
40
42a
24
28a
38
42c
22a
18
32a
12a

FIG. 2

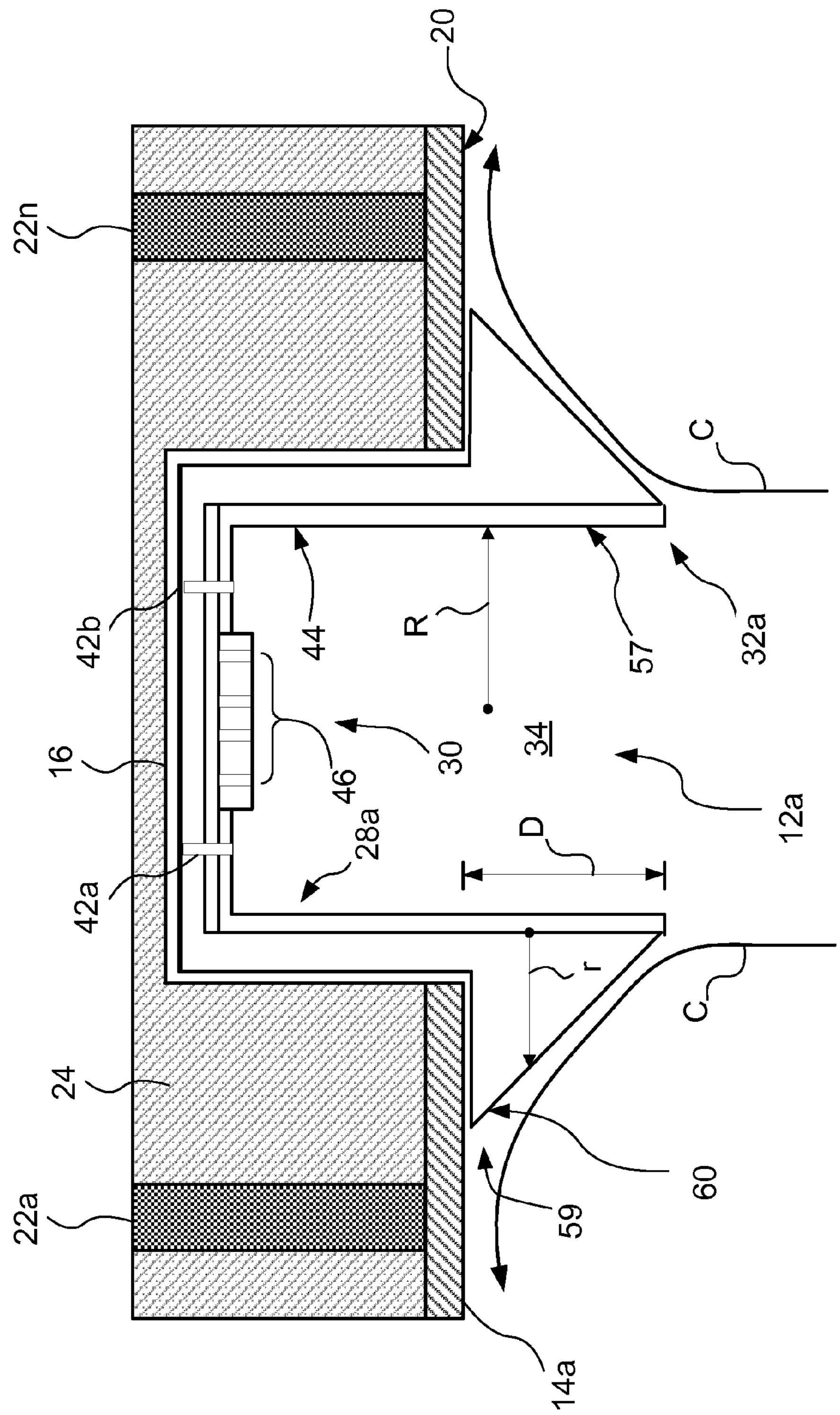
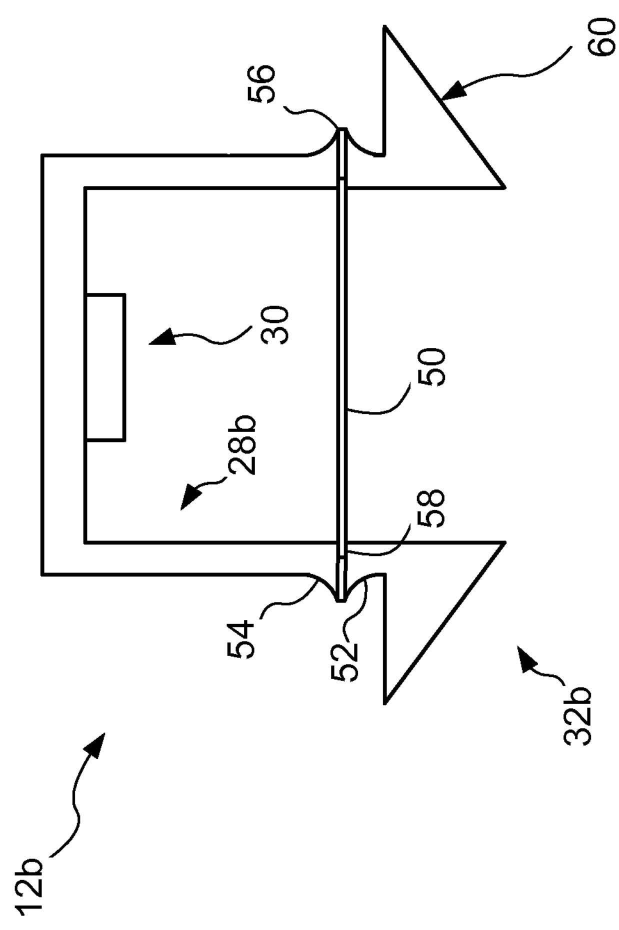


FIG. 3

FIG. 4



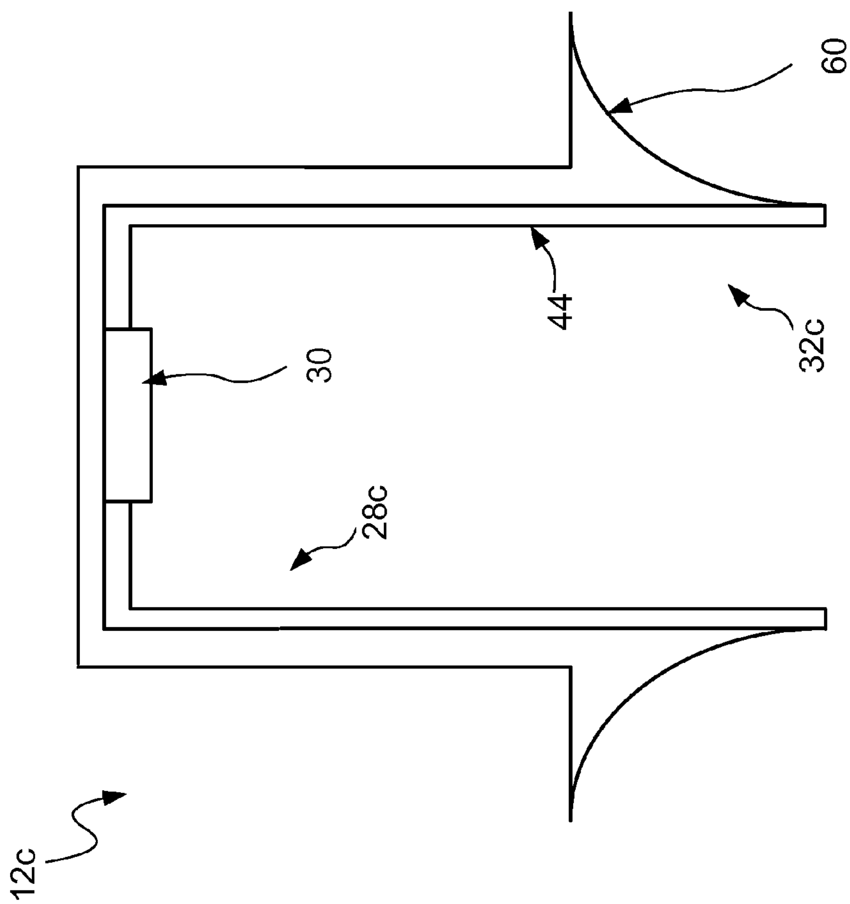
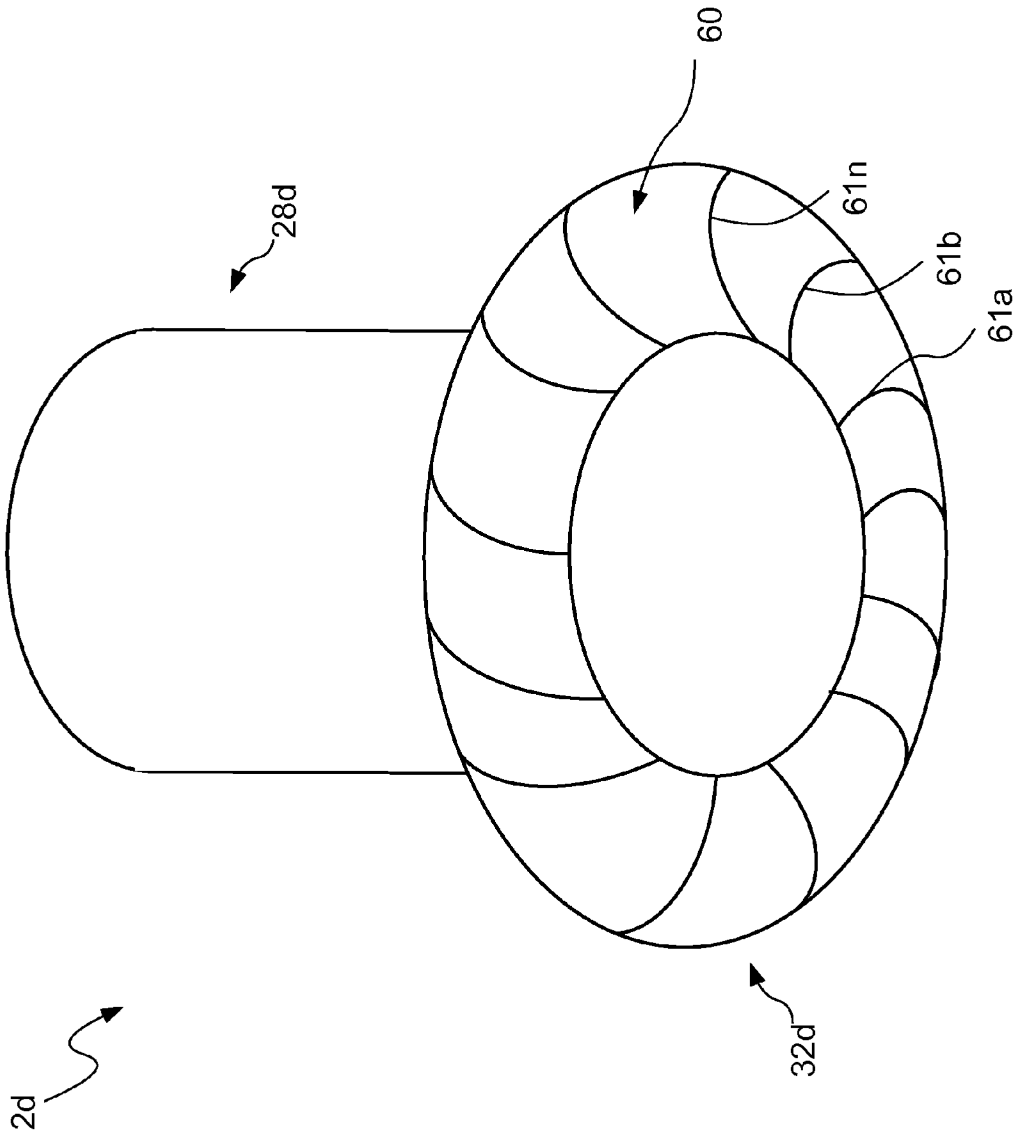


FIG. 5

FIG. 6



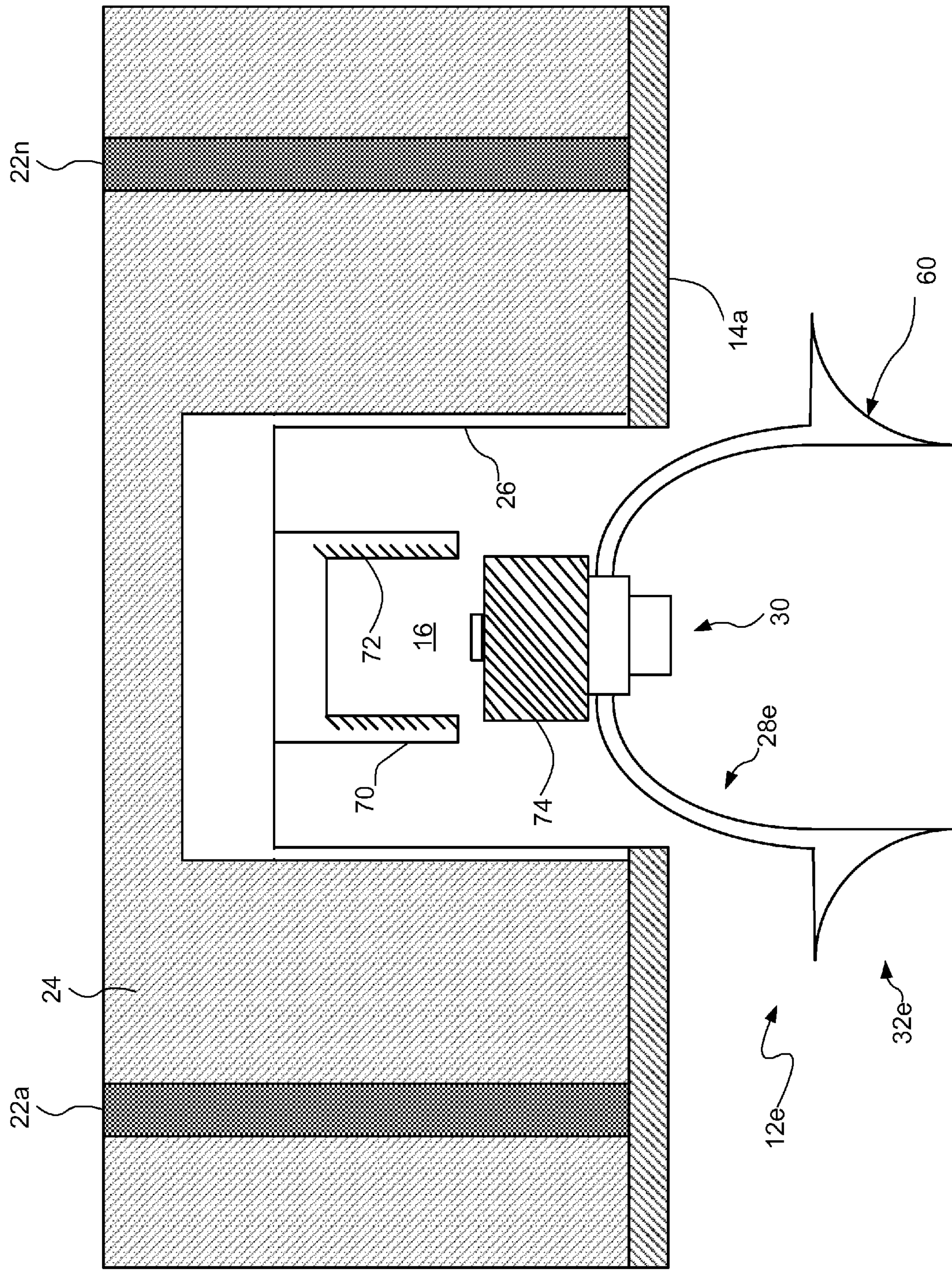


FIG. 7

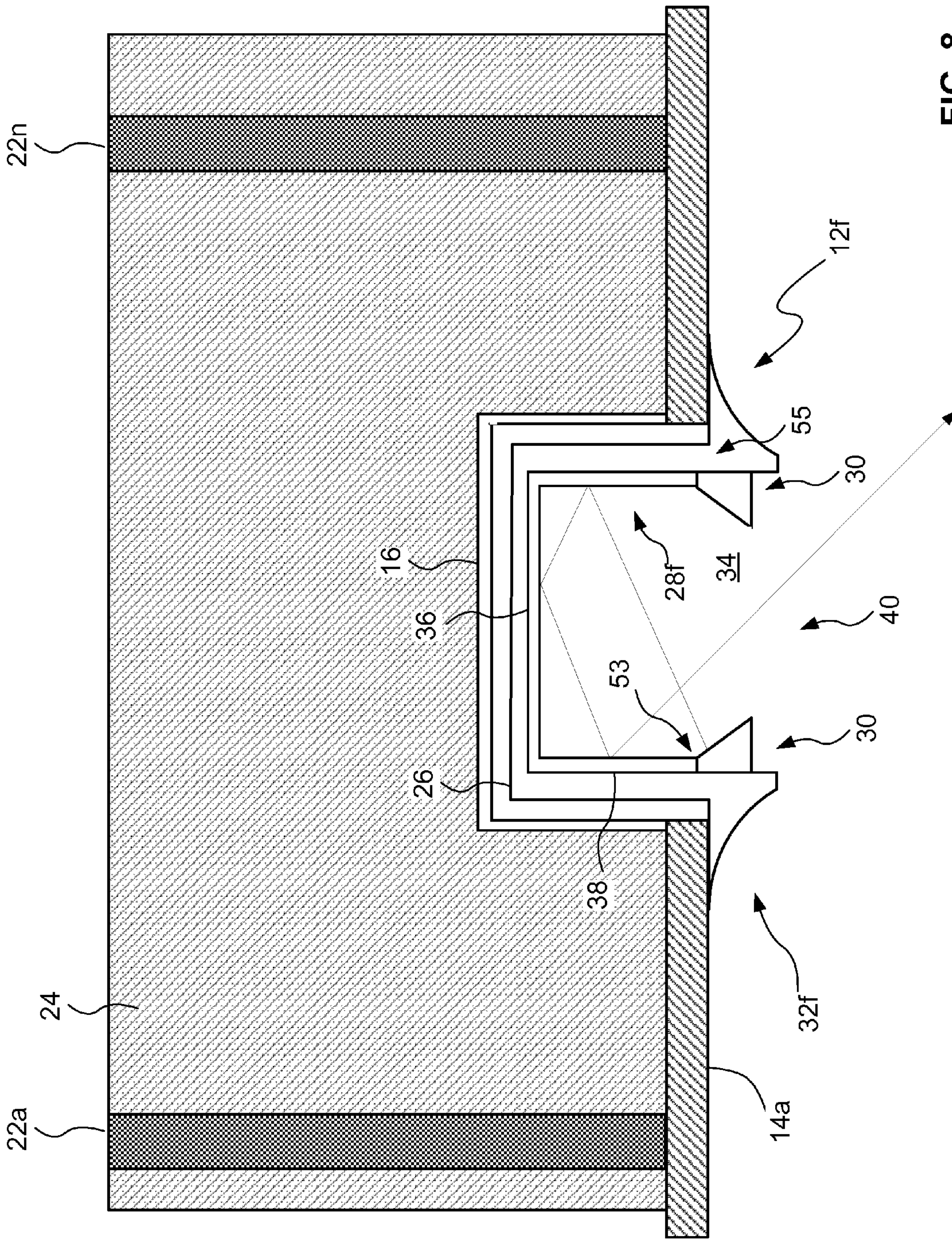


FIG. 8

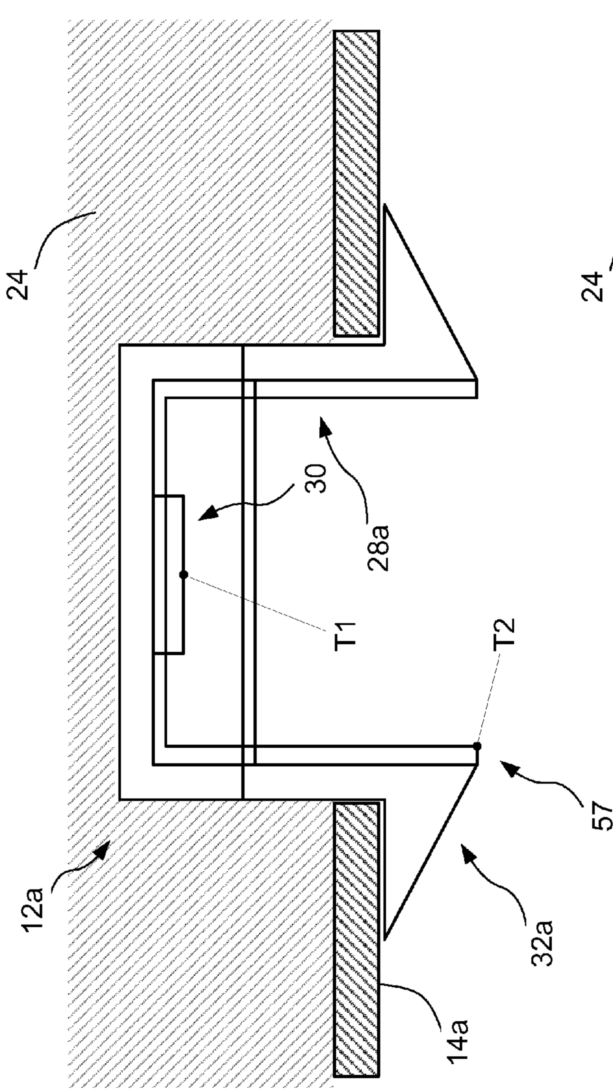


FIG. 9A

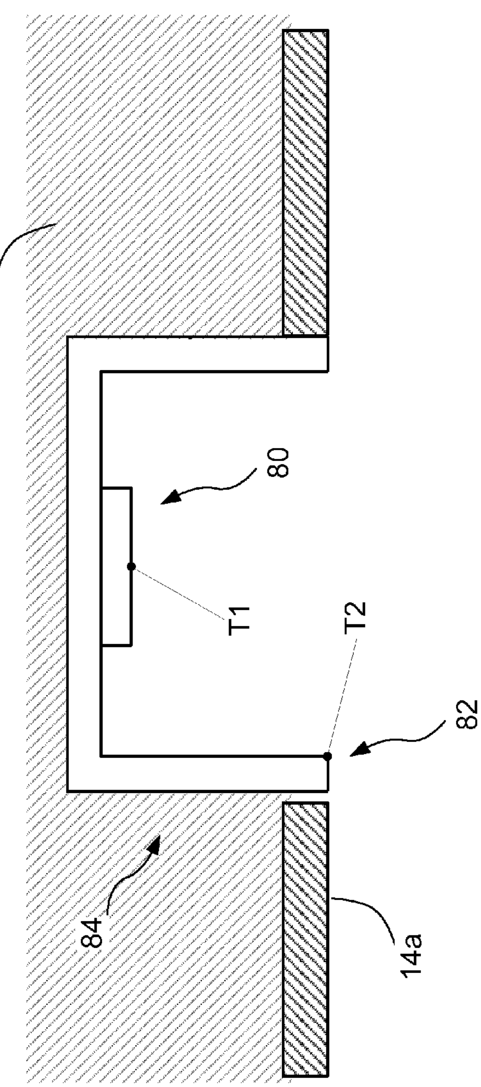
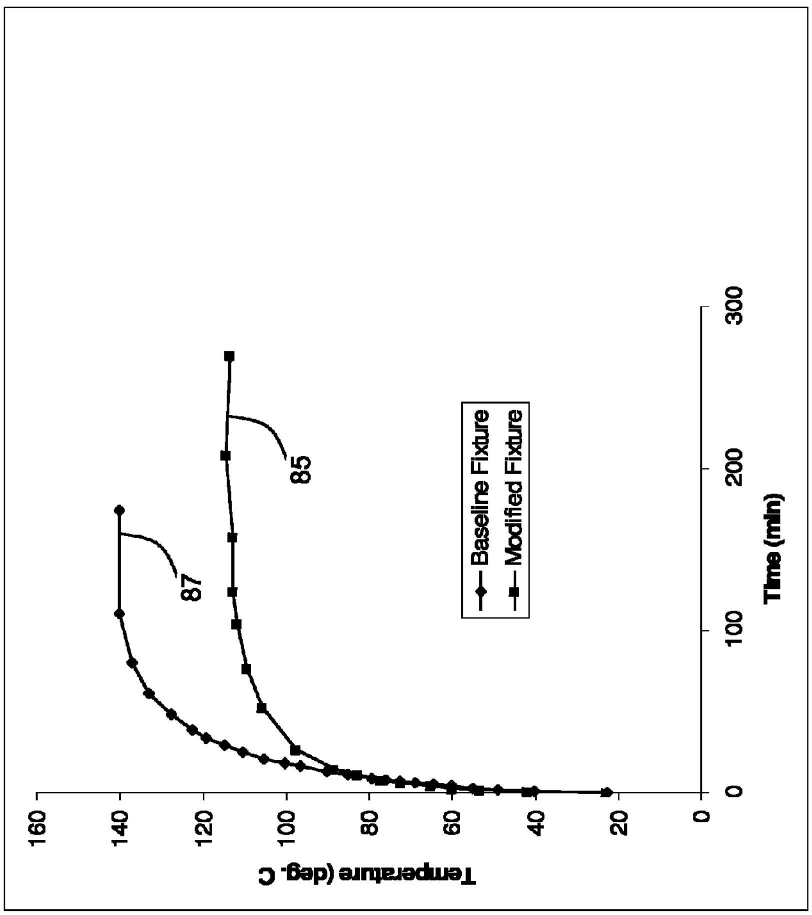


FIG. 9B

FIG. 10


Temperature (deg. C
160
140
120
100
80
60
40
20
0
Time (min)
0
100
200
300
Baseline Fixture
Modified Fixture
87
85

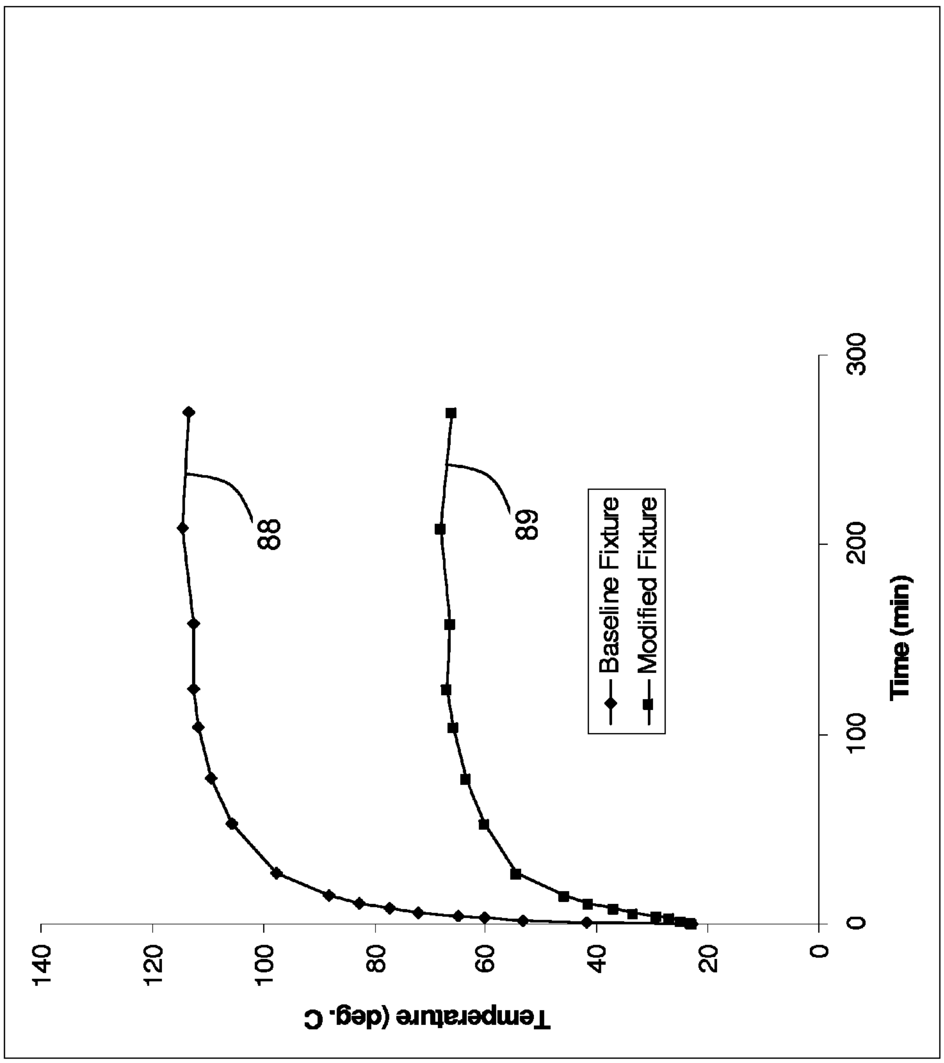

Temperature (deg. C
140
120
100
80
60
40
20
0
0
100
200
300
Time (min)
Baseline Fixture
Modified Fixture
88
89

FIG. 11

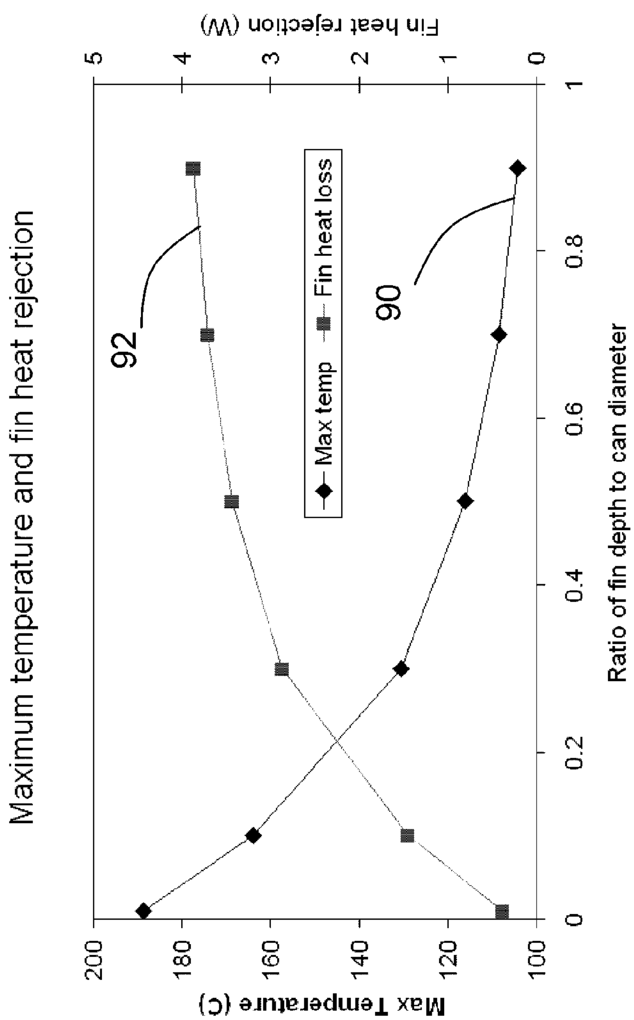

Maximum temperature and fin heat rejection
Max Temperature (C)
200
180
160
140
120
100
Fin heat rejection (W)
5
4
3
2
1
0
0
0.2
0.4
0.6
0.8
1
Ratio of fin depth to can diameter
Max temp
Fin heat loss
92
90

FIG. 12

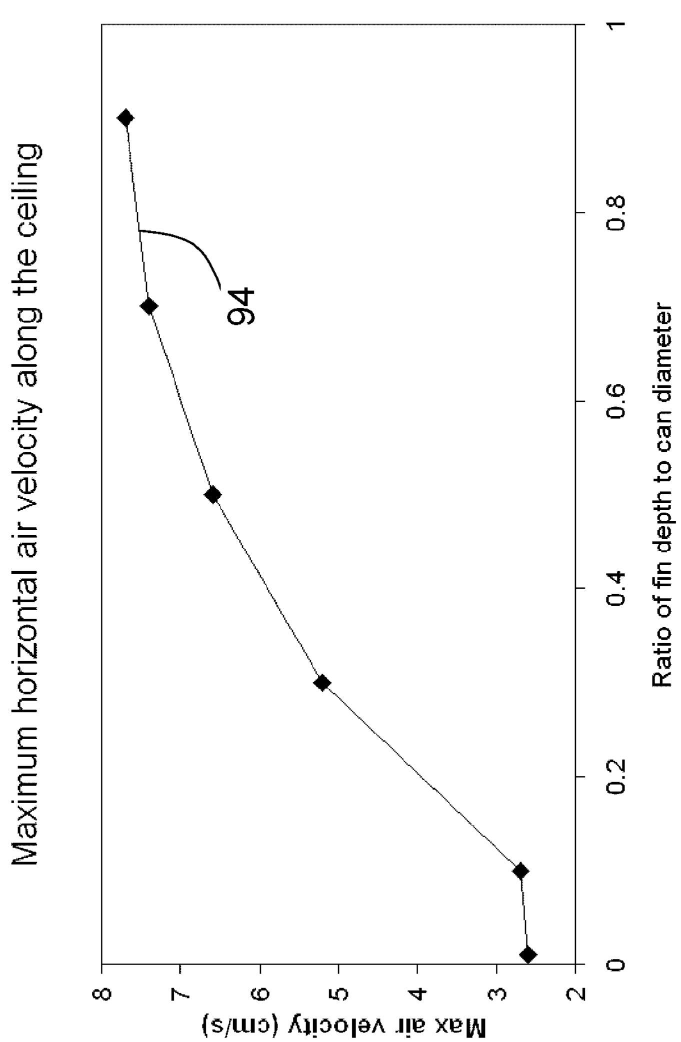

Maximum horizontal air velocity along the ceiling
Max air velocity (cm/s)
Ratio of fin depth to can diameter
94
8
7
6
5
4
3
2
0
0.2
0.4
0.6
0.8
1

FIG. 13

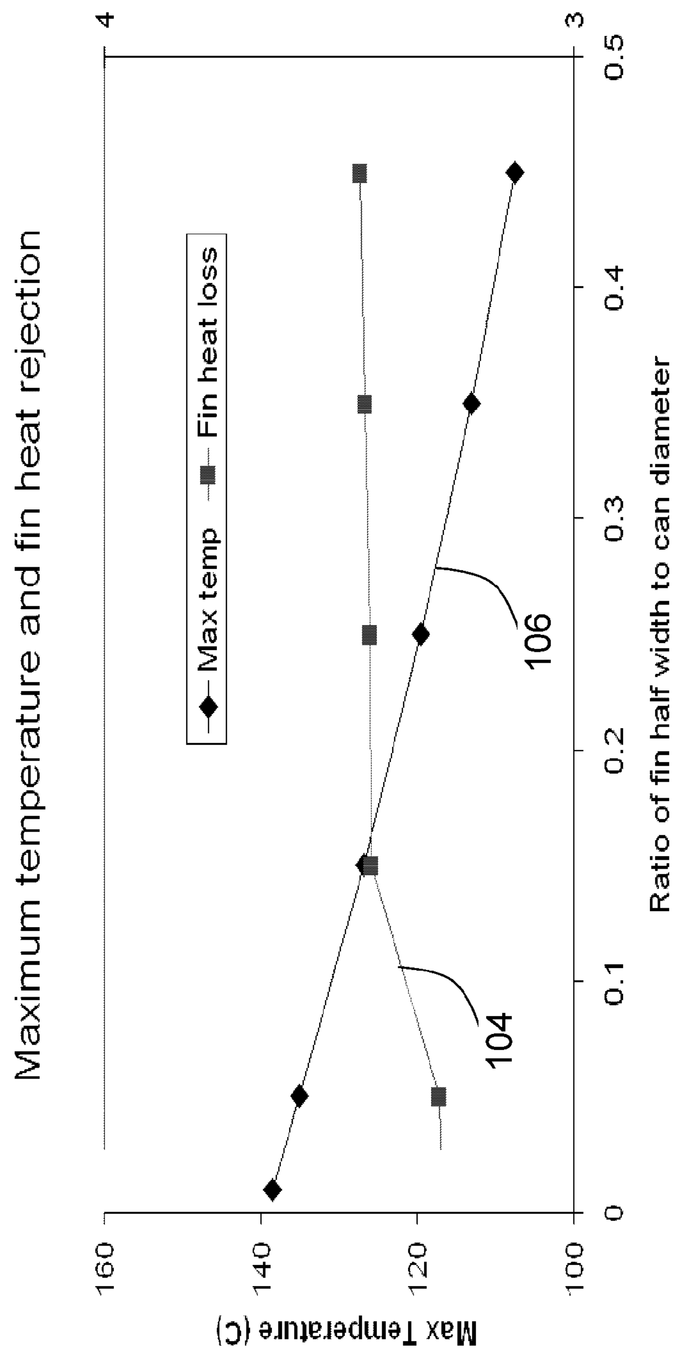

Maximum temperature and fin heat rejection
Max temp
Fin heat loss
Max Temperature (C)
Fin heat rejection (W)
Ratio of fin half width to can diameter
160
140
120
100
4
3
0
0.1
0.2
0.3
0.4
0.5
104
106

FIG. 14

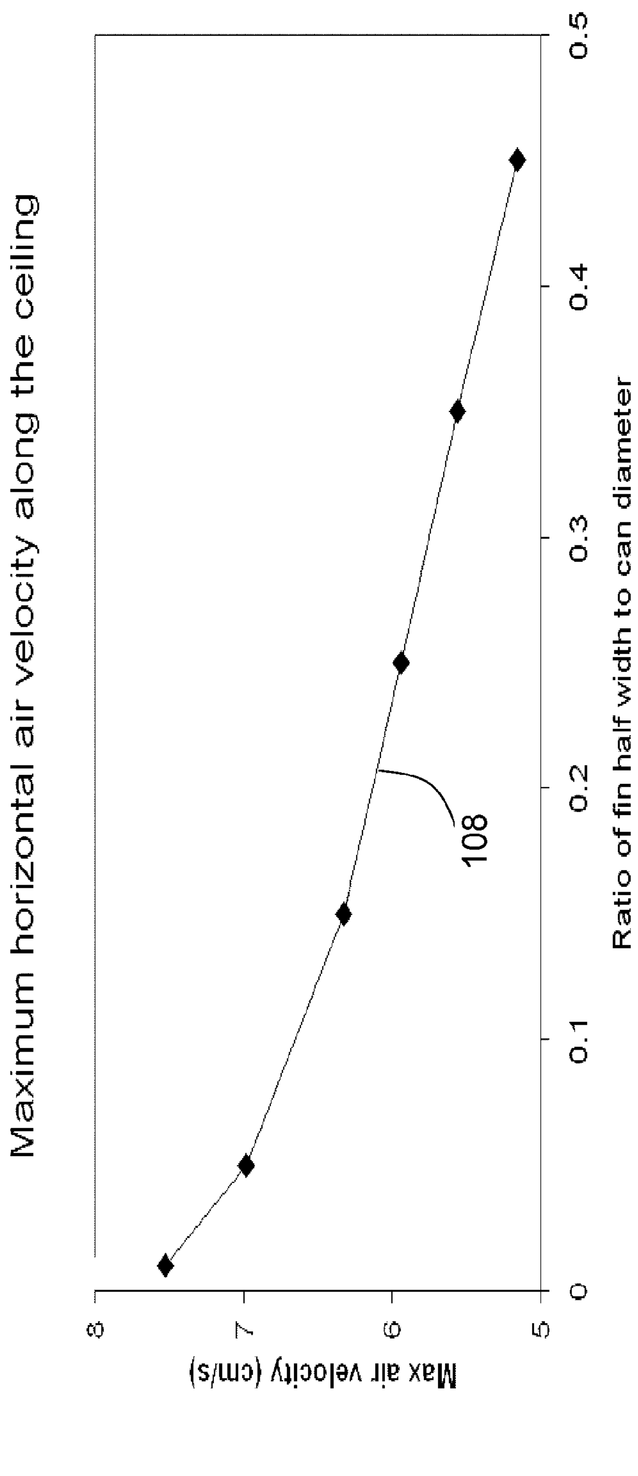

Maximum horizontal air velocity along the ceiling
Max air velocity (cm/s)
8
7
6
5
Ratio of fin half width to can diameter
0
0.1
0.2
0.3
0.4
0.5
108

FIG. 15

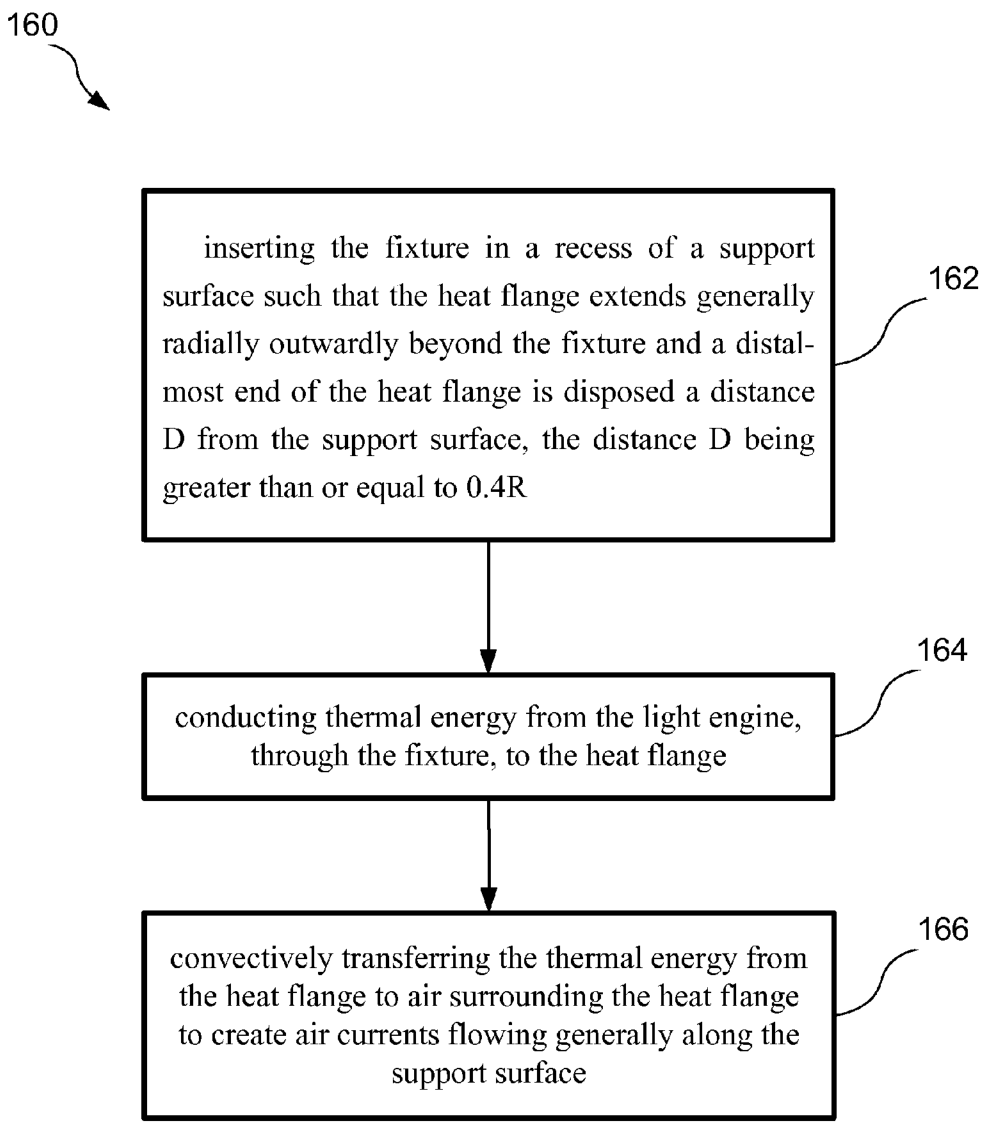

160
inserting the fixture in a recess of a support surface such that the heat flange extends generally radially outwardly beyond the fixture and a distal-most end of the heat flange is disposed a distance D from the support surface, the distance D being greater than or equal to 0.4R
162
conducting thermal energy from the light engine, through the fixture, to the heat flange
164
convectively transferring the thermal energy from the heat flange to air surrounding the heat flange to create air currents flowing generally along the support surface
166

FIG. 16

PARTIALLY RECESSED LUMINAIRE

CROSS-REFERENCE TO RELATED APPLICATIONS

This application is related to copending application, U.S. patent application Ser. No. 13/076,141, PARTIALLY RECESSED LUMINAIRE, filed simultaneously herewith, the entire disclosure of which is incorporated herein by reference.

TECHNICAL FIELD

The present disclosure relates to luminaires, and more particularly pertains to luminaires and methods for reducing the junction temperature of a light engine.

BACKGROUND

Luminaires, such as down lights or the like, may include a can and a light engine disposed within a cavity defined by the can. The light engine includes a light source configured to generate light. One such type of light source includes light emitting diodes, LEDs. While LEDs may generate less thermal energy compared to traditional bulbs (e.g., incandescent light bulbs), LEDs nevertheless generate thermal energy which should be managed in order to control the junction temperature. A higher junction temperature generally correlates to lower light output, lower luminaire efficiency, and/or reduced life expectancy. Unfortunately, managing thermal energy is particularly challenging when designing ceiling fixtures because temperature gradients in a room send the hottest air closest to the ceiling. Moreover, thermal insulation installed in the ceiling, and particularly proximate to the ceiling fixture, may reduce and/or suppresses natural convection. For example, the thermal insulation may have a thermal conductivity of approximately 0.04 W/(m−K), and as a result, the thermal insulation may generally only permit the removal of thermal energy upward from the ceiling fixture by thermal conduction which occurs at a far slower rate than thermal convection above the ceiling.

Another challenge facing the design of ceiling fixtures involves a plurality of ceiling fixtures installed throughout a room. In particular, the ceiling fixtures which are surrounded by other ceiling fixtures (e.g., ceiling fixtures in the middle of the room) are most vulnerable to overheating as they are farthest from the walls (which may help to act as a heat sink). Moreover, nearby ceiling fixtures generate thermal energy which reduces and/or minimizes any lateral temperature gradient across the ceiling. As a result, thermal energy is generally limited to upward and downward. Because hot air rises, most of the thermal energy must travel through the insulated ceiling.

BRIEF DESCRIPTION OF THE DRAWINGS

Features and advantage of the claimed subject matter will be apparent from the following description of embodiments consistent therewith, which description should be considered in conjunction with the accompanying drawings, wherein:

FIG. **1** is a block diagram of one exemplary embodiment of a system consistent with the present disclosure;

FIG. **2** is a cross-sectional view of one embodiment of a luminaire consistent with the present disclosure;

FIG. **3** is a cross-sectional view of the luminaire of FIG. **2** received within a recess of a support surface consistent with the present disclosure;

FIG. **4** is a cross-sectional view of another embodiment of a luminaire consistent with the present disclosure;

FIG. **5** is a cross-sectional view of yet another embodiment of a luminaire consistent with the present disclosure;

FIG. **6** is a cross-sectional view of a further embodiment of a luminaire consistent with the present disclosure;

FIG. **7** is a cross-sectional view of another embodiment of a retrofit luminaire consistent with the present disclosure;

FIG. **8** is a cross-sectional view of another embodiment of a luminaire consistent with the present disclosure;

FIGS. **9**A and **9**B are cross-sectional views illustrating the placement of thermocouples T**1** and T**2**;

FIG. **10** depicts a comparison of the temperatures of the thermocouples T**1** in a partially-recessed luminaire consistent with the present disclosure and a flush-mounted luminaire;

FIG. **11** depicts a comparison of the temperatures of the thermocouples T**2** in a partially-recessed luminaire consistent with the present disclosure and a flush-mounted luminaire;

FIG. **12** depicts the maximum temperature and heat rejection as function of the ratio of the heat flange depth to the cavity is varied;

FIG. **13** depicts the maximum horizontal air velocity as the ratio of depth of the heat flange to the cavity is varied;

FIG. **14** depicts the maximum temperature and heat rejection as a function of the ratio of the flange half-width r to normalized diameter of luminaire;

FIG. **15** depicts the maximum horizontal air velocity along the ceiling as a function of the normalized luminaire diameter; and

FIG. **16** is a block flow diagram of one exemplary method consistent with the present disclosure.

DETAILED DESCRIPTION

By way of an overview, one aspect consistent with the present disclosure may feature a luminaire including a fixture, a light engine coupled to the fixture, and a heat flange configured to extend outwardly beyond the mounting surface of the luminaire. The heat flange reduces the junction temperature of the light engine by increasing the amount of convection in the surrounding air, thereby increasing the volumetric air flow across the fixture as well as the air velocity. As used herein, the term "junction temperature" is intended to refer to the maximum temperature of the light engine when operating at steady state power. In particular, thermal energy is conductively transferred from the light engine, through the fixture, to the heat flange where the thermal energy is convectively transferred from the heat flange to surrounding air to create air currents flowing along the support surface. The increased volumetric air flow and velocity transfers a greater amount of thermal energy from the fixture into the surrounding air, thereby reducing the junction temperature of the light engine. In addition, the shape of the heat flange increases the air velocity across the mounting surface of the luminaire, thereby exposing the heated air to a larger area of the mounting surface, and reducing the temperature difference needed to transfer the thermal energy from the air to the mounting surface. Reducing the junction temperature of the light engine may increase the life expectancy of the light engine and/or may allow the light engine to be operated at a higher luminance while also maintaining an acceptable service life.

Turning now to FIG. **1**, one embodiment illustrating a lighting system **10** consistent with the present disclosure is generally illustrated. The lighting system **10** includes at least one partially-recessed luminaire **12** coupled, mounted, fixed, or otherwise secured to at least one mounting substrate **14**_a-n_. For the sake of brevity, the partially-recessed luminaire **12** (also referred to simply as "luminaire") will be described as a being coupled to a ceiling **14***a*; however, it will be appreciated that the luminaire **12** may also be coupled to any mounting substrate **14***a*-*n* such as, but not limited to, a wall **14***b*, floor **14***n*, roof, or the like.

Referring now to FIGS. **2** and **3**, a cross-sectional view of one embodiment of a luminaire **12***a* for use with a ceiling **14***a* is generally illustrated. The luminaire **12***a* may be configured to be at least partially received in a recess **16** formed within the ceiling **14***a*, for example, as generally illustrated in FIG. **3**. The ceiling **14***a* may include an exterior layer **18** (for example, but not limited to, sheet rock, wood, a dropped ceiling, or the like) having a bottom surface **20**, at least one stud or support **22***a*-*n*, and optionally insulation **24** (such as, but not limited to, thermal and/or sound insulation). As used herein, the exterior layer **18** and bottom surface thereof are intended to refer to the layer and surface of the ceiling **14***a* which are exposed to the area illuminated by the luminaire **12**. Optionally, the recess **16** may include an electrical box **26** depending on the building codes. For example, the electrical box **26** may include any electrical box compatible with UL® or the like. One or more electrical wires (not shown for clarity) may be provided to supply AC and/or DC current to the luminaire **12**. The recess **16** and/or electrical box **26** may have any shape such as, but not limited to, a generally square, generally rectangular, or generally circular shape.

The luminaire **12***a* includes a fixture **28***a*, a light engine **30** configured to be coupled to the fixture **28***a*, and a heat flange **32***a* configured to extend outwardly beyond the bottom surface **20** of the ceiling **14***a* when the luminaire is fully received in the recess as shown in FIG. **3**. The fixture **28***a* may define a cavity **34** having a base **36**, at least one sidewall **38**, and an open end **40**. The fixture **28***a* may be made from a material with a high thermal conductivity such as, but not limited to, a material having a thermal conductivity of 100 W/(m*K) or greater, for example, 200 W/(m*K) or greater. According to one embodiment, the fixture **28***a* may include a metal or metal alloys (such as, but not limited to, aluminum, copper, silver, gold, or the like), plastics (e.g., but not limited to, doped plastics), as well as composites. The size, shape and/or configuration (e.g., surface area) of the fixture **28***a* may depend upon a number of variables including, but not limited to, the maximum power rating of the light engine **30**, the size/shape of the recess **16** and/or electrical box **26**, and the like.

The fixture **28***a* may include one or more mounting devices **42***a*-*n* for securing the luminaire **12***a* to the recess **16** and/or electrical box **26**. The mounting devices **42***a*-*n* may include one or more openings or passages **42***a, b* extending through the fixture **28***a* for receiving a fastener (such as, but not limited to, a screw, bolt, or the like, not shown for clarity) which may engage a corresponding feature of the recess **16** and/or electrical box **26** (also not shown for clarity). Alternatively (or in addition), the mounting device **42***a*-*n* may include one or more biasing devices (such as, but not limited to, biased tabs, springs, or the like **42***c*) configured to engage a portion of the sidewalls of the recess **16** and/or electrical box **26**.

Optionally, the fixture **28***a* may include one or more surface layers **44** covering at least a portion of the internal surface of at least one of the base **36** and sidewall **38**. The surface layers **44** may include an optical coating configured to reflect and/or direct light generated from the light engine **30** out the open end **40**. For example, the optical coating may include a reflector and/or a lens configured to direct and/or focus light emitted from the light engine **30** out of the open end **40** of the luminaire **12***a*. Alternatively (or in addition), the surface layers **44** may include a thermal layer configured to increase the amount of thermal energy transferred from the light engine to the heat flange **32***a*. For example, the thermal layer may also have a high thermal conductivity, k, (e.g., but not limited to, a thermal conductivity, k, of 1.0 W/(m*K) or greater) to transfer thermal energy from the light engine **30** into the fixture **28***a* and to the heat flange **32***a*, thereby reducing the junction temperature of the light engine **30**. The fixture **28***a* may also optionally include a lens and/or diffuser **50** extending across the open end **40** configured to diffuse the light emitted from the light engine **30**.

The light engine **30** may include any light source including, but not limited to, gas discharge light sources (such as, but not limited to, high intensity discharge lamps, fluorescent lamps, low pressure sodium lamps, metal halide lamps, high pressure sodium lamps, high pressure mercury-vapor lamps, neon lamps, and/or xenon flash lamps) as well as one or more solid-state light sources (e.g., but not limited to, semiconductor light-emitting diodes (LEDs), organic light-emitting diodes (OLED), or polymer light-emitting diodes (PLED), hereinafter collectively referred to as "LEDs **46**"). The number, color, and/or arrangement of LEDs **46** may depend upon the intended application/performance of the luminaire **12***a*. The LEDs **46** may be coupled and/or mounted to a substrate (e.g., but not limited to, a ballast, PCB or the like **48**). The PCB **48** may comprise additional circuitry (not shown for clarity) including, but not limited to, resistors, capacitors, etc., which may be operatively coupled to the PCB **48** configured to drive or control (e.g., power) the LEDs **46**. According to one embodiment, the PCB **48** may be directly coupled to the fixture **28***a*. For example, a first surface **49** of the PCB **48** may contact or abut against a surface **51** of the fixture **28***a* to conduct thermal energy away from the LEDs **46**.

Optionally, the light engine **30** also includes one or more thermal interface materials (e.g., gap pads, not shown for clarity) disposed between the PCB **48** and the fixture to decrease the contact thermal resistance between the PCB **48** (and LEDs **46**) and the fixture **28***a*. The thermal interface material may include outer surfaces which directly contact (e.g., abut against) surfaces **49**, **51** of the PCB **48** and the fixture **28***a*, respectively. The thermal interface material may include a material having a higher thermal conductivity, k, configured to reduce the thermal resistance between the PCB **48** and the fixture **28***a*. For example, the thermal interface material may have a thermal conductivity, k, of 1.0 W/(m*K) or greater, 1.3 W/(m*K) or greater, 2.5 W/(m*K) or greater, 5.0 W/(m*K) or greater, 1.3-5.0 W/(m*K), 2.5-5.0 W/(m*K), or any value or range therein. The thermal interface material may include a deformable (e.g., a resiliently deformable) material configured to reduce and/or eliminate air pockets between the outer surfaces **49**, **51** of the PCB **48** and the fixture **28***a* to reduce contact resistance. The thermal interface material may have a high conformability to reduce interface resistance

The interface material may have a thickness of from 0.010" to 0.250" when uncompressed. Optionally, one or more outer surfaces of the first thermal interface material may include an adhesive layer configured to secure the thermal interface material to the PCB **48** or the fixture **28***a*, respectively. The adhesive may be selected to facilitate thermal energy transfer (e.g., the adhesive may have a thermal conductivity k of 1 W/(m*K) or greater. Additionally (or alternatively), the PCB **48** and the fixture **28***a* may be coupled (e.g., secured) together using one or more fasteners such as, but not limited to, screws, rivets, bolts, clamps, or the like. The thermal interface material may also be electrically non-conductive (i.e., an electrical insulator) and may include a dielectric material.

As discussed above, the luminaire **12**a also includes a heat flange **32**a coupled to the fixture **28**a. The heat flange **32**a may be made from a material having a high thermal conductivity (such as, but not limited to, a material having a thermal conductivity of 100 W/(m*K) or greater, for example, 200 W/(m*K) or greater) configured to transfer thermal energy away from the fixture **28**a, thereby reducing the junction temperature of the LEDs **46** that make up the light engine **30**. According to one embodiment, the fixture **28**a may include a metal or metal alloys (such as, but not limited to, aluminum, copper, silver, gold, or the like), plastics (e.g., but not limited to, doped plastics), as well as composites. The heat flange **32**a may be the same as the fixture **28**a or a different material than the fixture **28**a.

The heat flange **32**a may include a hollow, generally conical frustum shape having a generally circular cross-section which generally linearly tapers radially outwardly from the distal-most end **57** towards the fixture **28**a. Put another way, the half-width r of the conical heat flange **32**a (i.e., the flange half-width r) increases from the distal-most end **57** to proximal-most end **59** of the heat flange **32**a. As used herein, the term "generally conical frustum" is intended to mean that the top and base of the cone may be, but do not necessarily have to be, parallel to each other.

The distal-most end **57** of the heat flange **32**a also extends downwardly a depth D beyond the bottom surface **20** of the ceiling **14**a. The depth D of the heat flange **32**a may be selected such that the heat flange **32**a has a surface area large enough to transfer enough thermal energy from the heat flange **32** to the surrounding air by thermal convection to create an air current (as represented by arrows C) across the tapered exterior surface **60** of the heat flange **32**a. The shape of the heat flange **32**a also generates air currents C that flow upwardly across the heat flange **32**a and radially outwardly generally parallel to the bottom surface **20** of the ceiling **14**a. Because the heated air currents C flow generally along the bottom surface **20** of the ceiling **14**a, a larger area of the ceiling **14**a is exposed to the heated air currents C, thereby reducing the temperature differential needed to transfer thermal energy from the heated air currents C to the ceiling **14**a. The net result is that more thermal energy is transferred from the light engine **30** to the air, and ultimately to the ceiling **14**a, thereby reducing the junction temperature of the light engine **30**.

According to one embodiment, the heat flange **32**a has a depth D equal to or greater than 0.4 times the radius R of the fixture **28**a (i.e., equal to or greater than 0.2 times the diameter of the fixture **28**a). For example, the depth D may be equal to or greater than 0.6 times the radius R of the fixture **28**a (i.e., equal to or greater than 0.3 times the diameter of the fixture **28**a); equal to or greater than 0.8 times the radius R of the fixture **28**a (i.e., equal to or greater than 0.4 times the diameter of the fixture **28**a); and/or equal to or greater than 1.2 times the radius R of the fixture **28**a (i.e., equal to or greater than 0.6 times the diameter of the fixture **28**a). Alternatively, the depth D of the heat flange **32**a may be selected to be greater than or equal to 0.4R and less than or equal to 2R; greater than or equal to 0.4R and less than or equal to 1.4R; greater than or equal to 0.8R and less than or equal to 1.6R; greater than or equal to 0.8R and less than or equal to 1.4R, and/or any value in between. It should be understood that all luminaires consistent with the present disclosure feature heat flanges having the above described relationships between the distance D and radius R.

The conical heat flange **32**a has a maximum flange half-width r equal to or greater than 0.4 times the radius R of the fixture **28**a. As used herein, the term "maximum flange half-width r" is intended to refer to the maximum radial distance of the heat flange **32**a. For example, the maximum flange half-width r may correspond to the radial distance of the heat flange **32**a at the proximal-most end **59** of the heat flange **32**a configured to be adjacent to the ceiling **14**a as generally illustrated. The conical heat flange **32**a may also have a maximum flange half-width r equal to or greater than the radius R of the fixture **28**a. It should be understood that all luminaires consistent with the present disclosure feature heat flanges having the above described relationships between the maximum flange half-width r and radius R.

Turning now to FIG. **4**, the luminaire **12**b may include a fixture **28**b, a light engine **30**, and a heat flange **32** coupled to the fixture **28**b, for example, using an adhesive, friction connection, and/or one or more fasteners (not shown for clarity). The heat flange **32**b includes the same material as the fixture **28**b or a different material than the fixture **28**b. Optionally, the luminaire **12**b may include one or more thermal interface materials **56** (e.g., gap pads) disposed between the fixture **28**b and the heat flange **32**b to further increase the rate of thermal energy transferred from the fixture **28**b to the heat flange **32**b (and ultimately away from the LEDs **46** and the PCB **48**, not shown in FIG. **4** for clarity). For example, the thermal interface material **56** may include outer surfaces which at least partially contact (e.g., abut against) at least a portion of the surfaces of the heat flange **32**b and/or the fixture **28**b. According to one embodiment, the thermal interface material **56** may be disposed between (and optionally abut against) one or more of the flanges **52**, **54** of the heat flange **32**b and the fixture **28**b, respectively.

The thermal interface material **56** may include a material having a reasonably high thermal conductivity, k, configured to reduce the thermal resistance between the heat flange **32**b and the fixture **28**b. For example, the thermal interface material **56** may have a thermal conductivity k of 1.0 W/(m*K) or greater, 1.3 W/(m*K) or greater, 2.5 W/(m*K) or greater, 5.0 W/(m*K) or greater, 1.3-5.0 W/(m*K), 2.5-5.0 W/(m*K), or any value or range therein. The thermal interface material **56** may include a deformable (e.g., a resiliently deformable) material configured to reduce and/or eliminate air pockets between the surfaces of the heat flange **32**b and the fixture **28**b to reduce contact resistance. The thermal interface material **56** may have a high conformability to reduce interfacial resistance.

The thermal interface material **56** may have a thickness of from 0.010" to 0.250" when uncompressed. Optionally, one or more outer surfaces of the thermal interface material **56** may include an adhesive layer (not shown for clarity) configured to secure the thermal interface material **56** to the fixture **28**b or the heat flange **32**b. Additionally (or alternatively), the fixture **28**b and the heat flange **32**b may be secured together using one or more fasteners (not shown for clarity) such as, but not limited to, screws, rivets, bolts, clamps, or the like. The interface material **56** may also be electrically non-conductive (i.e., an electrical insulator), and may include a dielectric material.

The heat flange **32**b and the fixture **28**b, when secured together, may optionally define a lens cavity **58** configured to receive at least a portion of the outer periphery of a lens/diffuser **50** such that the lens/diffuser **50** is sandwiched between the fixture **28**b and the heat flange **32**b. Of course, the lens/diffuser **50** may be secured between and/or to the fixture **28**b and/or heat flange **32**b in a variety of different manners. For example, while not an exhaustive list, the lens/diffuser **50** may be an integral component with the surface layer **44** and/or may be secured to the fixture **28**b and/or heat flange

32*b* using a fastener, adhesive, welding (e.g., but not limited to, ultrasonic welding), or the like (not shown for clarity).

Turning now to FIG. **5**, a cross-sectional view of another embodiment of a luminaire **12***c* is generally illustrated. The luminaire **12***c* includes a fixture **28***c*, a light engine **30**, and a heat flange **32***c* having a hollow, generally conical frustum shape having a generally circular cross-section which curves or flares radially outwardly from the distal-most end **57** towards the fixture **28***c*. The curved heat flange **32***c* may increase the area of the surface **60** of the heat flange **32***c* which is exposed to the surrounding air, thereby enhancing the air currents generated. As a result, more thermal energy may be transferred from the curved heat flange **32***c* compared to the straight heat flange **32***a* (e.g., as illustrated in FIGS. **2** and **3**) and the junction temperature of the light engine **30** may be further reduced.

Referring now to FIG. **6**, an end perspective view of yet another embodiment of a luminaire **12***d* is generally illustrated. The luminaire **12***d* includes a fixture **28***d*, a light engine **30** (not shown because of the view), and a heat flange **32***d* having one or more (e.g., a plurality) of fins **61***a-n* extending generally outwardly from the heat flange **32***d*. For example, the fins **61***a-n* may extend along a longitudinal axis of the luminaire **12***d*; however, the fins **61***a-n* may extend diagonally and/or perpendicular to the longitudinal axis of the luminaire **12***d*. The fins **61***a-n* may further increase the area of the surface **60** of the heat flange **32***d* which is exposed to the surrounding air, thereby transferring more thermal energy from the heat flange **32***d* compared to the straight heat flange **32***a* and further reducing the junction temperature of the light engine **30**. The heat flange **32***d* may have a generally straight cross-section (e.g., as generally illustrated in FIG. **2**) and/or a curved cross-section (e.g., as generally illustrated in FIG. **5**). The fins **61***a-n* may extend generally outwardly at a constant distance from the heat flange **32***d* and/or may have a tapered shape. The fins **61***a-n* may be evenly and/or unevenly spaced along the heat flange **32***d*. In addition, the fins **61***a-n* may have a generally pin-like or generally cylindrical shape.

Yet another embodiment of a luminaire **12***e* consistent with the present disclosure is generally illustrated in FIG. **7**. In particular, the luminaire **12***e* may be configured to be retrofitted to an existing light socket **70**. The light socket **70** may include an Edison screw-type light socket having a threaded socket **72** configured to receive a corresponding threaded portion **74** of the luminaire **12***e*. For example, the light socket **70** may include, but is not limited to, an E12, E11, E17, E14, E26, E27, E39, or and E40. The luminaire **12***e* may also include a fixture **28***e*, a light engine **30**, and a heat flange **32***e*. The heat flange **32***e* may include any heat flange consistent with the present disclosure.

Turning now to FIG. **8**, a cross-sectional view of yet a further embodiment of a luminaire **12***f* consistent with the present disclosure is generally illustrated. The luminaire **12***f* includes a fixture **28***f*, one or more light engines **30***f*, and a heat flange **32**. The heat flange **32***f* may include any heat flange consistent with the present disclosure. Rather than having the light engine **30** disposed at the base **36** of the fixture **28***f*, one or more light engines **30** may be coupled to the sidewalls **38** of the fixture **28***f* and/or the heat flange **32***f*. For example, the light engines **30** may be disposed proximate to the distal end **53** of the fixture **28***f* and/or the proximal end **55** of the heat flange **32***f*. The light engine **30** may be configured to emit light directly out the open end **40** of the luminaire **12***f* and/or emit light into the cavity **34** where it is reflect out the open end **40**. Placing the light engine **30** on the sidewalls **38** and/or the heat flange **32***f* may increase the amount of thermal energy which is transferred from the light engine **30** to the heat flange **32***f* and ultimately to the surrounding air, thereby reducing the junction temperature of the light engine **30**. While not shown, the luminaire **12***f* may also include one or more light engines coupled to the base **36** of the fixture **12***f*.

Experiments were performed on a luminaire **12***a* consistent with FIG. **3** as well as a flush-mounted luminaire. In particular, as generally illustrated in FIG. **9**A, a first and a second thermocouple T**1**, T**2** were placed on the light engine **30** (which was replace by a heater) and the proximal-most end **57** of a luminaire **12***a* consistent with FIG. **3**. Similarly, a first and a second thermocouple T**1**, T**2** were placed on the light engine **80** (which was replace by a heater) and the proximal-most end **82** of a flush-mounted luminaire **84** as generally illustrated in FIG. **9**B. The light engines **30**, **80** in both the luminaires **12***a*, **84** of FIGS. **9**A and **9**B generated 23 watts of thermal energy. While note shown, the luminaires **12***a*, **84** were also surrounded by insulation **24** to simulate a typical installation in a ceiling **14***a*. The temperature of the thermocouples T**1** and T**2** for each luminaire **12***a*, **84** was then recorded as a function of time as generally illustrated in FIGS. **10** and **11**.

In particular, FIG. **10** generally illustrates the temperature **85**, **87** of the first thermocouple T**1** in each luminaire **12**, **84**, respectively. As may be seen, the flush-mounted luminaire **84** of FIG. **9**B had a steady state temperature **87** of approximately 140 degrees C. after approximately 3-5 hours (steady state was assumed at the point when the temperature of the thermocouple T**1** stopped rising). In contrast, the luminaire **12***a* of FIG. **9**A had a steady state temperature **85** of approximately 115 degrees C. (a reduction of approximately 25 degrees C.).

Turning now to FIG. **11**, the temperature **88**, **89** of the second thermocouple T**2** in each luminaire **12***a*, **84**, respectively, is generally illustrated. As may be seen, the difference in the temperature **88**, **89** at T**2** between the luminaires **12***a*, **84** is even larger at the bottom **57**, **82** of the luminaires **12***a*, **84** than it is at the light engine **30**, **80**. While this result may at first seem counterintuitive, the reason is that much more thermal energy is removed from the partially-recessed luminaire **12***a* at the bottom (due to convection) than is removed from the flush-mounted luminaire **84**. The additional flow of thermal energy of the partially-recessed luminaire **12***a* imposes an additional temperature difference top-to-bottom in the partially-recessed luminaire **12***a*. As a result, the partially-recessed luminaire **12***a* runs approximately 40 degrees cooler at the bottom **57** compared to the bottom **82** of the flush-mounted luminaire **84**.

Turning now to FIGS. **12** and **13**, simulations were performed on a variety of luminaires having a flared heat flange (for example, a heat flange as generally illustrated in FIG. **5**) with different depths D. In particular, FIG. **12** generally illustrates the maximum temperature **90** of the light engine as a function of the normalized depth D of the heat flange. In addition, the maximum temperature **92** of the proximal-most end of the heat flange (i.e., the amount of thermal energy rejected from the heat flange to the air) was also recorded as a function of the normalized depth D of the heat flange. FIG. **13** generally illustrates maximum horizontal air velocity **94** along the ceiling as a function of the normalized depth D of the heat flange. As can be seen, the maximum horizontal air velocity **94** (FIG. **13**) increases significantly after the normalized depth D of the heat flange exceeds a ratio of approximately 0.2 (i.e., 0.4R). The increased thermal energy rejection **92** and corresponding lower temperature **90** of FIG. **12** is due to the combined effects of the higher air velocity **94** of FIG. **13** and the larger exposed surface area of the heat flange.

As illustrated in FIGS. **14** and **15**, simulations were also performed on a variety of luminaires having a flared heat flange (for example, a heat flange as generally illustrated in FIG. **5**) with different flange half-widths r. In particular, FIG. **14** generally illustrates the maximum temperature **104** of the light engine as a function of the ratio of the flange half-width r to diameter of luminaire (normalized by the normalized by the luminaire diameter). Note, that luminaire diameter is equal to 2R. In addition, the maximum temperature **106** of the proximal-most end of the heat flange (i.e., the amount of thermal energy rejected from the heat flange to the air) was also recorded as a function of the normalized luminaire diameter. FIG. **15** generally illustrates maximum horizontal air velocity **108** along the ceiling as a function of the normalized luminaire diameter.

FIG. **16** is a block flow diagram of one method **160** of reducing the junction temperature of a luminaire consistent with the present disclosure. The luminaire includes a fixture defining a cavity, a light engine, and a heat flange. The fixture is inserted **162** into a recess of a support surface such that the heat flange extends generally radially outwardly beyond the fixture and a distal-most end of the heat flange is disposed a distance D from the support surface, the distance D being greater than or equal to 0.4R. Thermal energy is conducted **164** from the light engine, through the fixture, to the heat flange. The thermal energy is convectively transferred **166** from the heat flange to the air surrounding the heat flange to create air currents flowing generally along the support surface.

While the block flow diagram for FIG. **16** may be shown and described as including a particular sequence of steps. It is to be understood, however, that the sequence of steps merely provides an example of how the general functionality described herein can be implemented. The steps do not have to be executed in the order presented unless otherwise indicated.

Thus, a luminaire consistent with the present disclosure may reduce the junction temperature. The luminaire may be particularly useful in applications where vertical convection above the ceiling and/or lateral convection inside the room are suppressed. The luminaire may also be particularly useful in applications with stagnant or near stagnant air floor within a room. The luminaire may therefore run at a lower temperature with the same power (i.e., luminance) compared to a flush-mounted luminaire (thus increasing the life-expectancy of the light engine) or at a higher power with the same temperature compared to a flush-mounted luminaire while also maintaining an acceptable service life. A luminaire may include a fixture, at least one light engine coupled to the fixture, and a heat flange coupled to the fixture. The heat flange is configured to extend below the support surface a distance D, wherein D is greater than or equal to 0.4 times the radius of the fixture.

The present disclosure recognizes that the insulation above a luminaire in a common installation reduces the transfer of thermal energy from the luminaire and may create a bottleneck. The partially-recessed luminaire of the present disclosure reduces and/or eliminates this bottleneck by increasing the surface area of the ceiling which is used to transfer the thermal energy from the luminaire. In particular, the heat flange reduces the junction temperature of the light engine by increasing the amount of convection in the surrounding air, thereby increasing the volumetric air flow across the fixture as well as the air velocity. In particular, thermal energy is conductively transferred from the light engine, through the fixture, to the heat flange where the thermal energy is convectively transferred from the heat flange to surrounding air to create air currents flowing along the support surface. The shape of the heat flange directs the heated air outwardly away from the luminaire and generally along the surface of the support surface. This heated air is then exposed to a greater area of the support surface (i.e., the heat-flow area). Because the cross-sectional area of heat flow through the support surface is so much larger due to the increased air currents generated by the heat flange, the temperature differential required to transfer the thermal energy into the support surface is much smaller. The increased volumetric air flow and velocity transfers a greater amount of thermal energy from the fixture into the surrounding air, thereby reducing the junction temperature of the light engine.

According to one aspect, the present disclosure may feature a luminaire including a fixture, a light engine, and a heat flange. The fixture is configured to be generally received in a recess of a support surface and defines a cavity having a radius R. The light engine is configured to be disposed within the cavity and includes at least one light source. The heat flange is disposed about a distal end region of the fixture. The heat flange has a generally conical cross-section extending generally radially outwardly beyond the fixture and extending away from the distal end region of the fixture. A distal-most end of the heat flange is configured to be disposed a distance D from the support surface when the fixture is received in the recess. The distance D is greater than or equal to 0.4R

According to another aspect, the present disclosure may feature a luminaire including a fixture, and a heat flange. The fixture is configured to be generally received in a recess of a support surface and defines a cavity having a radius R. The cavity is configured to receive at least one light engine. The heat flange has a generally conical cross-section extending generally radially outwardly beyond the fixture. A distal-most end of the heat flange is configured to be disposed a distance D from the support surface when the fixture is received in the recess. The distance D is greater than or equal to 0.4R.

According to yet another aspect, the present disclosure may feature a method of reducing the junction temperature of a luminaire including a fixture defining a cavity, a light engine, and a heat flange. The method includes inserting the fixture in a recess of a support surface such that the heat flange extends generally radially outwardly beyond the fixture and a distal-most end of the heat flange is disposed a distance D from the support surface, the distance D being greater than or equal to 0.4R; conducting thermal energy from the light engine, through the fixture, to the heat flange; and convectively transferring the thermal energy from the heat flange to air surrounding the heat flange to create air currents flowing generally along the support surface.

The terms "first," "second," "third," and the like herein do not denote any order, quantity, or importance, but rather are used to distinguish one element from another, and the terms "a" and "an" herein do not denote a limitation of quantity, but rather denote the presence of at least one of the referenced item.

While the principles of the present disclosure have been described herein, it is to be understood by those skilled in the art that this description is made only by way of example and not as a limitation as to the scope of the invention. The features and aspects described with reference to particular embodiments disclosed herein are susceptible to combination and/or application with various other embodiments described herein. Such combinations and/or applications of such described features and aspects to such other embodiments are contemplated herein. Other embodiments are contemplated within the scope of the present invention in addition to the exemplary embodiments shown and described herein. Modifications and substitutions by one of ordinary skill in the art are considered to be within the scope of the present invention, which is not to be limited except by the following claims.

What is claimed is:

1. A luminaire for direct installation in a ceiling comprising:

a fixture configured to be generally received directly in a recess of a ceiling support surface for direct installation of the luminaire in the ceiling, said fixture defining a cavity having a radius R;

a light engine configured to be disposed within said cavity, said light engine comprising at least one light source; and

a heat flange disposed about a distal end region of said fixture, said heat flange having multiple fins having a generally conical frustum shape extending generally radially outwardly and downwardly beyond said fixture and extending away from said distal end region of said fixture beyond a bottom surface of the ceiling in a vertical direction and extending outward from the distal end region of said fixture in a horizontal direction, wherein a distal-most end of said heat flange is configured to be disposed a distance D from said support surface when said fixture is received in said recess, said distance D being greater than or equal to 0.4R and the fixture and the heat flange are one integral, single piece of material.

2. The luminaire of claim **1**, wherein said generally conical frustum shape has a cross-section of said heat flange generally linearly tapers radially outwardly from a proximal end region of the heat flange to said distal-most end of said heat flange.

3. The luminaire of claim **1**, wherein said heat flange has a curved, generally conical cross-section.

4. The luminaire of claim **3**, wherein said curved, generally conical cross-section is concaved.

5. The luminaire of claim **3**, wherein said curved, generally conical cross-section is convex.

6. The luminaire of claim **1**, wherein said fixture and said heat flange is a monolithic component formed from the same piece of metal.

7. The luminaire of claim **1**, wherein said heat flange and said fixture is constructed of a single monolithic molded structure.

8. The luminaire of claim **1**, wherein said heat flange and said fixture comprise the same material providing a continuous, uninterrupted path of thermal conductivity from said fixture to said heat flange.

9. The luminaire of claim **1**, wherein said heat flange and said fixture providing a direct, uninterrupted path of thermal conductivity from said fixture to said heat flange.

10. The luminaire of claim **7**, further comprising a thermal interface between said heat flange and said fixture, said thermal interface comprising a material having a thermal conductivity, k, of at least 1.0 W/(m*K).

11. The luminaire of claim **1**, wherein said distance D is greater than or equal to 0.6R.

12. The luminaire of claim **1**, wherein said distance D is greater than or equal to 0.8R.

13. The luminaire of claim **1**, wherein said distance D is less than or equal to 2R.

14. The luminaire of claim **1**, wherein said light engine comprises at least one light emitting diode.

15. The luminaire of claim **1**, wherein said light engine is coupled to a base region of said cavity.

16. The luminaire of claim **1**, wherein said light engine is disposed proximate to said distal end region of said fixture proximate to said heat flange.

17. The luminaire of claim **1**, further comprising a wire coupled to said light engine of said fixture, said wire configured to be coupled to an electric box external to said luminaire.

18. A luminaire comprising:

a fixture configured to be generally received directly in a recess of a ceiling support surface, said fixture defining a cavity having a radius R, wherein said cavity is configured to receive at least one light engine; and

a heat flange consisting of multiple fins extending generally radially outwardly beyond said fixture wherein the multiple fins extend from a distal end region of said fixture beyond a bottom surface of the ceiling support surface in a vertical direction downward and extend outward, perpendicular to the ceiling support surface in a radial pattern extending away from a center axis of the fixture, and wherein said fixture and said heat flange are one integral structure constructed of the same material.

19. A recessed ceiling can for direct installation in an insulated ceiling comprising:

a fixture configured to be generally be received directly in a ceiling recess and couple directly to a support surface of the ceiling, said fixture defining a cavity having a radius R;

a light engine configured to be disposed within said cavity, said light engine comprising at least one light source and wire power leads from said at least one light source extending external to said recessed ceiling can for direct wire connection to an electrical box; and

a heat flange disposed about a distal end region of said fixture, said heat flange having multiple fins having a generally conical frustum shape extending generally radially outwardly beyond said fixture and extending away from said distal end region of said fixture, beyond a bottom surface of the ceiling wherein multiple fins extending generally outwardly from said heat flange and said multiple fins run vertically and substantial perpendicular to and below the bottom surface of the ceiling wherein said multiple fins extend in a spoke like manner in planes that intersect in a vertical line running along a center axis of the fixture wherein said generally conical frustum shape has a cross-section of said heat flange generally linearly tapers radially outwardly from a proximal end region of the heat flange to said distal-most end of said heat flange.

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